



**Addendum y to
ASHRAE Guideline 36-2018**

Public Review Draft

Proposed Addendum y to Guideline 36-2018, High-Performance Sequences of Operation for HVAC Systems

Second Public Review (April 2021)

(Draft shows Proposed Independent Substantive Changes to Previous Public Review Draft)

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(This foreword is not part of this guideline. It is merely informative and does not contain requirements necessary for conformance to the guideline.)

FOREWORD

This addendum includes the ~~HW plant sequences and associated logic variables and hardwired control points developed as part of ASHRAE Research Project 1711: Advanced Sequences of Operation for HVAC Systems—Phase II Central Plants and Hydronic Systems. Typos and minor language clarity issues identified since final publication of the RP-1711 sequences on December 31, 2019 have been cleaned up in this version.~~ is the second public review of addendum y addressing control sequences for Hot Water Plants and includes only substantive changes to the first public review draft. Rationale for each change is shown directly before the change.

Cross references herein refer to content from Addendum r. Approval of this addendum is therefore predicated on approval of Addendum r.

Note: This public review draft makes proposed independent substantive changes to the previous public review draft. These changes In this addendum, changes to the current guideline are indicated in the text by underlining (for additions) and strikethrough (for deletions) unless the instructions specifically mention some other means of indicating the changes. Only these changes are open for review and comment at this time. Additional material is provided for context only and is not open for comment except as it relates to the proposed substantive changes.

Addendum y to Guideline 36-2018

**This addendum version assumes Addendum x adoption.*

Revise Section 3.1.8.4 as follows to clarify that QbX is not limited to condensing boilers and is the output capacity.

Retain the following parameter for plants with non-condensing boilers. Delete otherwise.

- a. QbX, design output capacity of Boiler X, in KBtu/h.

Add Section 3.1.8.5 to include variables for the number of pumps for clarity. Renumber the rest of this section accordingly.

3.1.8.5. Headered Pump Design Quantities

Retain the following parameters if primary hot water pumps are headered.

- a. N-PHWP, the number of primary hot water pumps that operate at design conditions

Retain the following parameters if secondary hot water pumps are headered.

- b. N-SHWP, the number of secondary hot water pumps that operate at design conditions

Revise Section 4.11.1. to no longer list firing rate as a required point; sequences use calculated load for staging instead since firing rate is not always available.

4.11.1. Boilers

Required?	Description	Type	Device
R	Boiler enable	DO	Connect to boiler enable contact; typ. each boiler
R	HW supply temperature setpoint	AO	AI to boiler control panels or AI through boiler network interfaces.
<u>Optional point for monitoring boiler firing rate.</u>			
R RO	Boiler firing rate	AI	Firing rate from boiler controller (may be via network connection rather than hardwired). Use gas valve position if firing rate is not known. Typ. each boiler.

Revise Section 4.11.3. to clarify that minimum flow bypass is not required for boilers that do not have a minimum flow rate such as high mass boilers.

4.11.3. Primary HW Loop

Required?	Description	Type	Device
HW flow required for primary-only plants; the flow meter must be located on the plant side of the HW minimum flow bypass where provided. Optional for variable primary-variable secondary plants. Not required nor recommended for constant primary-variable secondary plants.			
A	HW supply or return flow	AI	Flow meter
HW bypass valve is required for variable flow primary-only plants <u>with boilers with non-zero minimum flow.</u> Delete otherwise.			
A	HW Min flow bypass valve	AO	Modulating valve sized for minimum flow of one boiler

Delete Section 5.21.3.7 since noncondensing boilers are not staged on minimum firing rate.

Retain the following clause for hybrid plants. Delete otherwise.

~~5.21.3.7. Non-condensing boilers in hybrid boiler plants are staged in part based on the capacity output of operating non-condensing boilers alone. $Q_{Non-Cond}$ is calculated as the sum of boiler firing rate times design capacity, Q_{bX} , for all operating non-condensing boilers.~~

~~The non-condensing boiler primary loop in hybrid boiler plants typically does not have a flow meter, so capacity output is estimated based on firing rate and design capacity.~~

Modify Section 5.21.3.9.f to be more conservative when staging boilers on to ensure they do not end up cycling off; cycling losses are much larger than the efficiency improvement of running condensing boilers at part load.

f. Stage up if any of the following is true:

1. **Availability Condition:** The equipment necessary to operate the current stage are unavailable. The availability condition is not subject to the minimum stage runtime requirement. Or
2. **Efficiency Condition:** Both of the following are true:

5. $Q_{required}$ exceeds ~~150~~200% of $B-STAGE_{MIN}$ of the next available stage for 10 minutes
 - iii. Hot water flowrate exceeds the minimum flow setpoint of the next available stage (see 5.21.8).
- 3. Failsafe Condition:** HW supply temperature is $10^{\circ}\text{F} < \text{setpoint}$ for 15 minutes.
- g. Stage down if all of the following are true:
 1. Either:
 - i. $Q_{required}$ falls below 110% of $B-STAGE_{MIN}$ of the current stage for 5 minutes; or
 - ii. The minimum flow bypass valve, if provided, is greater than 0% open for 5 minutes.
 2. The failsafe stage up condition is not true.
 3. $Q_{required}$ is less than 80% of the design capacity, Q_{bX} , of the boilers in the next available lower stage for 5 minutes.

Condensing boilers are generally more efficient at low load since the ratio of heat transfer surface area to thermal mass flowrate is maximized, increasing flue gas condensation. Staging on boilers at low load therefore maximizes plant efficiency. However, the energy penalty from cycling losses due to staging on lag equipment prematurely, only to have them cycle off, may more than offset the part load efficiency gains.

Staging is delayed until the current stage output exceeds the minimum output of the next stage by ~~50~~100% to avoid boiler short cycling following stage up, which dramatically decreases plant efficiency. The default stage up ~~ing~~ threshold for the efficiency condition is set ~~intentionally high~~ to ensure sufficient load to prevent boilers from short cycling and to create an adequate hysteresis to prevent unnecessary boiler staging, but the optimal threshold will depend in part on the boiler turndown. The designer should consider adjusting this threshold based on plant attributes: higher for boilers with more turndown, lower for boilers with less turndown.

Modify Section instructions for Ssections 5.21.3.10. and 5.21.3.11 which are not used for hybrid plants. Hybrid plants are covered under Clauses 5.21.3.12 through 5.21.3.17.

Retain the following two clauses for plants with only condensing or non-condensing boilers. Delete the following two clauses for hybrid plants.

~~5.21.3.11-5.21.3.10.~~ Whenever a lag boiler is enabled:

Revise Section 5.21.6.4 and 5.21.7.3 to reference a variable for the number of pumps, which has been added as a parameter in Section 3.

- 5.21.6.4. HW pumps shall be staged as a function of the ratio of current hot water flow, $FLOW_P$, to design flow, $PHWF_{design}$, and the number of pumps, N_{PHWP} , that operate at design conditions. Pumps are assumed to be equally sized.

$$HWFR = \frac{FLOW_P}{PHWF_{design}}$$

- 5.21.7.3. Secondary HW pumps shall be staged as a function of SHWFR, the ratio of current hot water flow, $FLOW_S$, to design flow, and the number of pumps, N_{SHWP} , that operate at design conditions. Pumps are assumed to be equally sized.

$$SHWFR = \frac{FLOW_S}{SHWF_{design}}$$

Revise Sections 5.21.11.4.b and 5.21.11.6, revising variable name from HWFlow_{B-X} to HWFlowStatus_{B-X}.

Retain the following fault condition if there is a flow meter in the primary loop. Delete otherwise. Duplicate the following fault condition for each primary loop with a flow meter.			
FC#2	Equation	$FLOW_{P,AVG} > \epsilon_{FM}$ and $Status_{PHWP} = \text{Off}$	Applies to OS #1
	Description	Primary hot water flow is too high with the hot water pumps off	
	Possible Diagnosis	Flow meter error	
Retain the following fault condition for primary-secondary plants with a flow meter in the secondary loop. Delete otherwise. Duplicate the following fault condition for each secondary loop flow meter.			
FC#3	Equation	$FLOW_{S,AVG} > \epsilon_{FM}$ and $Status_{SHWP} = \text{Off}$	Applies to OS #1
	Description	Secondary hot water flow is too high with the associated hot water pumps off	
	Possible Diagnosis	Flow meter error	
Retain the following fault condition for primary-secondary plants and primary-only plants where pump speed is controlled to maintain differential pressure. Delete otherwise. Duplicate the following fault condition for each differential pressure sensor and/or each secondary loop where pump speed is controlled to maintain differential pressure.			
FC#4	Equation	$DP_{AVG} < DPSP - \epsilon_{DP}$ and $Speed_{HWP} \geq 99\% - \epsilon_{VFDSPD}$	Applies to OS #2, #3
	Description	Hot water loop differential pressure is too low with hot water pump(s) at full speed.	
	Possible Diagnosis	Problem with VFD Mechanical problem with pump(s) Pump(s) are undersized Differential pressure setpoint is too high HWST is too low Primary flow is higher than the design flow of the operating boilers	
Retain the following fault condition for primary-only plants with a minimum flow bypass valve. Delete otherwise.			
FC#5	Equation	$FLOW_{P,AVG} < HW\text{-}MinFlowSp - \epsilon_{FM}$ and $MFBPV \geq 99\% - \epsilon_{MFBPV}$	Applies to OS #2, #3
	Description	Primary hot water flow is too low with the minimum flow bypass valve fully open.	
	Possible Diagnosis	Problem with minimum flow bypass valve Problem with boiler isolation valves Minimum loop differential pressure setpoint too low	
For hybrid plants, duplicate the following fault condition for each primary loop.			

FC#6	Equation	$HWST_{AVG} + \epsilon_{HWT} < HWSTSP$	Applies to OS #2, #3
	Description	Hot water supply temperature is too low.	
	Possible Diagnosis	Mechanical problem with boilers Primary flow is higher than the design flow of the operating boilers Deviation between the internal boiler hot water supply temperature sensor and the plant hot water supply temperature is too high (i.e. boiler sensor is out of calibration).	
Retain the following fault condition for plants where system gauge pressure is monitored. Delete otherwise.			
FC#7	Equation	$P_{GAUGE, AVG} < 0.9 * ETPreChargePress$	Applies to OS #1 – #3
	Description	Hot water system gauge pressure is too low	
	Possible Diagnosis	Possible hot water system leak	
Retain the following fault condition for plants with a condensing boiler. Delete otherwise.			
FC#8	Equation	$HWRT_{AVG} - \epsilon_{HWT} > CondTemp$	Applies to OS #2, #3
	Description	Hot water return temperature is too high for condensing to occur.	
	Possible Diagnosis	Hot water supply temperature setpoint is too high. Hot water load is too low. High bypass flow is raising the entering water temperature. Hot water coils are not designed for condensing at current loads.	
Retain the following fault condition for plants with a non-condensing boiler. Delete otherwise.			
FC#9	Equation	$HWRT_{AVG} + \epsilon_{HWT} < CondTemp$	Applies to OS #2, #3
	Description	Hot water return temperature is too low. Condensing is likely to occur.	
	Possible Diagnosis	Hot water supply temperature setpoint is too low.	
Retain the following fault condition if any boiler has a network interface and the plant has a common hot water supply temperature sensor at the discharge of the boiler(s). Delete otherwise. For hybrid plants, duplicate the following fault condition for each primary loop.			
FC#10	Equation	$ \frac{(\sum(HW-Flow_{StatusB-X} * HWST_{B-X}) / \sum HW-Flow_{StatusB-X}) - HWST_{AVG}}{\epsilon_{HWT}} > \epsilon_{HWT}$	Applies to OS #2
	Description	Deviation between the active boiler hot water supply temperature and the common hot water supply temperature is too high.	
	Possible Diagnosis	A hot water supply temperature sensor is out of calibration	
Retain the following fault condition if any boiler has a network interface and the plant has a common hot water return temperature sensor at the inlet of the boiler(s). Delete otherwise. For hybrid plants, duplicate the following two fault condition for each primary loop.			
FC#11	Equation	$ \frac{(\sum(HW-Flow_{StatusB-X} * HWRT_{B-X}) / \sum HW-Flow_{StatusB-X}) - HWRT_{AVG}}{\epsilon_{HWT}} > \epsilon_{HWT}$	Applies to OS

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